

## 107(a): Thomas Precession from the Commutator of Lorentz Boosts

In UFT406 it was shown that the Euler theory has been fixed entirely because of its neglect of geodetic and Lense-Thirring precessions when considering planetary orbits. This leaves the Thomas precession as the only correct theory of planetary precession. In ECE2 theory it can be derived from the commutator of ECE2 "variant" boosts. These have the same mathematical structure as the well known Lorentz boosts, but are defined in a space with finite curvature and torsion.

### Boost Matrix in the X Direction

This is defined by:

$$B_x = \begin{bmatrix} \cosh \phi & \sinh \phi & 0 & 0 \\ \sinh \phi & \cosh \phi & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} \gamma & \gamma \beta & 0 & 0 \\ \gamma \beta & \gamma & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad (1)$$

where

$$\beta = \frac{v}{c}, \quad \gamma = \left(1 - \frac{v^2}{c^2}\right)^{-1/2} \quad (2)$$

This connects two inertial frames, moving with relative speed  $v$ . If the relative motion is along the  $X$  axis, then:

$$\left. \begin{aligned} X' &= \gamma(X + vt) \\ Y' &= Y \\ Z' &= Z \\ t' &= \gamma(t + vX/c^2) \end{aligned} \right\} \quad (3)$$

The boost generator along  $X$  is:

$$K_x = \frac{1}{i} \frac{\partial B_x}{\partial \phi} \Big|_{\phi=0} = -i \begin{bmatrix} 0 & 1 & 0 & 0 \\ 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} \quad (4)$$

### Boost Matrix in the Y Direction

In this case the relative motion is along  $Y$ , so

$$\left. \begin{aligned} X' &= X \\ Y' &= \gamma(Y + vt) \\ Z' &= Z \\ t' &= \gamma(t + vY/c^2) \end{aligned} \right\} - (5)$$

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$$B_Y = \begin{bmatrix} \gamma & 0 & \gamma\beta & 0 \\ 0 & 1 & 0 & 0 \\ \gamma\beta & 0 & \gamma & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} \cosh\phi & 0 & \sinh\phi & 0 \\ 0 & 1 & 0 & 0 \\ \sinh\phi & 0 & \cosh\phi & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} - (6)$$

The boost generator is:

$$K_Y = \frac{1}{i} \begin{bmatrix} 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 \\ 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} - (7)$$

Boost Matrix in the Z Direction  
In this case:

$$\left. \begin{aligned} X' &= X \\ Y' &= Y \\ Z' &= \gamma(Z + vt) \\ t' &= \gamma(t + vZ/c^2) \end{aligned} \right\} - (8)$$

The boost matrix is:

$$B_Z = \begin{bmatrix} \gamma & 0 & 0 & \gamma\beta \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ \gamma\beta & 0 & 0 & \gamma \end{bmatrix} = \begin{bmatrix} \cosh\phi & 0 & 0 & \sinh\phi \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ \sinh\phi & 0 & 0 & \cosh\phi \end{bmatrix} - (9)$$

and the boost generator is

$$K_Z = \frac{1}{i} \begin{bmatrix} 0 & 0 & 0 & 1 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 1 & 0 & 0 & 0 \end{bmatrix} - (10)$$

It is shown in "The Enigmatic Photon" that:

$$[K_x, K_y] = -i J_z \quad (11)$$

of cyclicity

where the rotation generators are:

$$J_x = \frac{1}{i} \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 \\ 0 & 0 & -1 & 0 \end{bmatrix}, J_y = \frac{1}{i} \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & -1 \\ 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \end{bmatrix}, J_z = \frac{1}{i} \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & -1 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} \quad (12)$$

S. the commutator of ECE2 covariant Dirac is the ECE2 covariant rotation generator. This is the fundamental origin of the Thomas precession.

Proof

Consider the commutator:

$$B_x B_y - B_y B_x = \begin{bmatrix} 0 & \gamma\beta - \gamma^2\beta & \gamma^2\beta - \gamma\beta & 0 \\ \gamma^2\beta - \gamma\beta & 0 & \gamma^2\beta & 0 \\ \gamma\beta - \gamma^2\beta & -\gamma^2\beta & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} \quad (13)$$

$$= \gamma\beta \begin{bmatrix} 0 & -(\gamma-1) & \gamma-1 & 0 \\ \gamma-1 & 0 & \gamma\beta & 0 \\ -(\gamma-1) & -\gamma\beta & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix}$$

For a rotation of  $2\pi$ , the Thomas precession is:

$$\Delta\phi_T = 2\pi(\gamma-1) \quad (14)$$

Stress for the rotation about  $z$  of the ECE2 if fermion is element, as shown in previous notes and pgs.

For  $z$ , (14):

$$4) \quad 2\pi (B_x B_y - B_y B_x) = \gamma \beta \begin{bmatrix} 0 & -\Delta\phi_T & \Delta\phi_T & 0 \\ \Delta\phi_T & 0 & 2\pi\gamma\beta & 0 \\ -\Delta\phi_T & -2\pi\gamma\beta & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} \quad (15)$$

$$= \gamma \beta \left( \Delta\phi_T \left( \begin{bmatrix} 0 & -1 & 0 & 0 \\ 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} + \begin{bmatrix} 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 \\ -1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} \right) + 2\pi\gamma\beta \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & -1 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} \right)$$

This result shows that the commutator of boost matrices  $B_x$  and  $B_y$  produces rotations about  $X$ ,  $Y$  and  $Z$ . The commutator of boost generators however, produces a rotation only about  $Z$ .

Finally use the results:

$$\gamma' \beta' = \gamma^2 - 1 = (\gamma - 1)(\gamma + 1) \quad (16)$$

and

$$\gamma\beta = (\gamma^2 - 1)^{1/2} \quad (17)$$

From eq. (14):

$$\gamma = \frac{\Delta\phi_T}{2\pi} + 1 \quad (18)$$

so

$$\gamma' \beta' = \left( \frac{\Delta\phi_T}{2\pi} + 1 \right)^2 - 1 \quad (19)$$

$$\gamma\beta = \left( \left( \frac{\Delta\phi_T}{2\pi} + 1 \right)^2 - 1 \right)^{1/2} \quad (20)$$

Therefore the commutator can be expressed entirely  
terms of the Thomas precession,  $\Delta\phi_T$ .

The result for  $Z$  axis rotation from eq. (15)

is :

$$(B_x B_y - B_y B_x)_z = \gamma^2 \beta^2 \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & -1 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} - (21)$$

$$= \left( \left( \frac{\Delta \phi_T}{2\pi} + 1 \right)^2 - 1 \right) \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & -1 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix}$$

1) If there is no Thomas precession:  
 $\Delta \phi_T = 0 - (22)$

then there is no rotation:

$$(B_x B_y - B_y B_x)_z = 0 - (23)$$

2) In the low velocity limit:

$$\frac{\Delta \phi_T}{2\pi} \rightarrow \frac{1}{2} \left( \frac{v}{c} \right)^2 - (24)$$

so

$$(B_x B_y - B_y B_x)_z \rightarrow 2 \left( \frac{1}{2} \left( \frac{v}{c} \right)^2 \right) \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & -1 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} - (25)$$

this is the fundamental origin of the Thomas factor 1/2.  
 In deriving eq. (24) we have used.

$$\left( \frac{\Delta \phi_T}{2\pi} + 1 \right)^2 = \left( \frac{\Delta \phi_T}{2\pi} \right)^2 + 2 \left( \frac{\Delta \phi_T}{2\pi} \right) + 1 - (26)$$

$$\sim 2 \left( \frac{1}{2} \left( \frac{v}{c} \right)^2 \right) + 1$$